

# **Forging the Future of Iron: Energy, Economics, and Emissions**

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# Agenda



## Industry Background

Where today's iron comes from and what that means for emissions.



## Reduction Basics

How reducing gases convert iron ore into direct reduced iron.



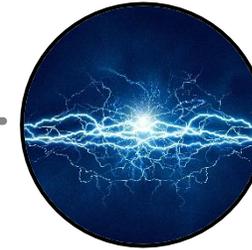
## Energy Sourcing

Decarbonization is an energy problem, not an ironmaking problem.



## Bioenergy Utilization

Charm Industrial's approach to novel bioenergy sourcing to secure new biogenic reducing gas.



## Novel Paths for Production

Other approaches to ironmaking that need to be considered.



## Route Comparison

Where do we go from here?

**AI Disclosure:** This presentation was developed with the assistance of generative AI. All factual data and citations have been independently verified against primary sources to ensure accuracy.



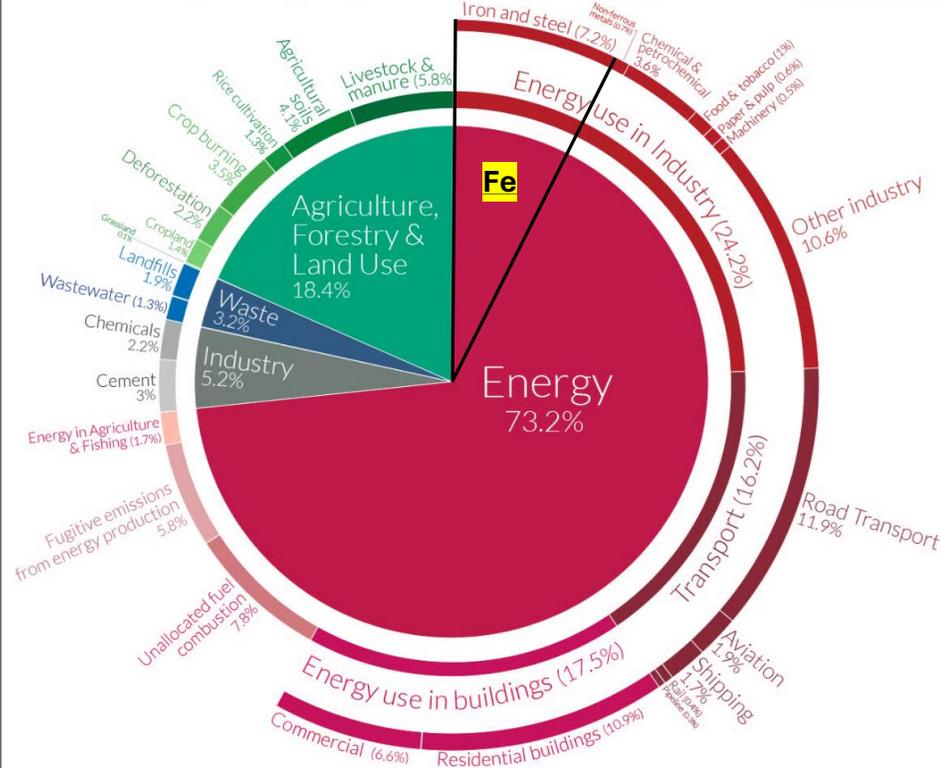
# We're Good at Making Iron Today – Why Discuss Alternatives?

The global iron and steel industry is one of the world's largest producers of greenhouse gases including CO<sub>2</sub><sup>1</sup>

## Global greenhouse gas emissions by sector

This is shown for the year 2016 – global greenhouse gas emissions were 49.4 billion tonnes CO<sub>2</sub>eq.

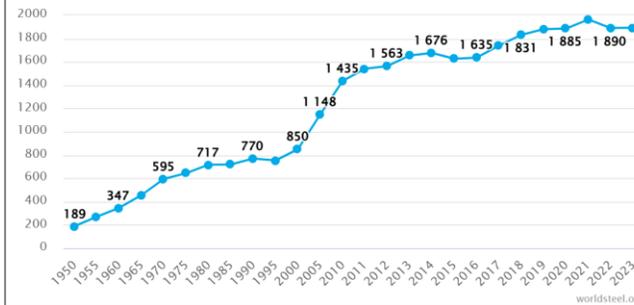
Our World in Data



OurWorldinData.org – Research and data to make progress against the world's largest problems. Source: Climate Watch, the World Resources Institute (2020). Licensed under CC-BY by the author Hannah Ritchie (2020).

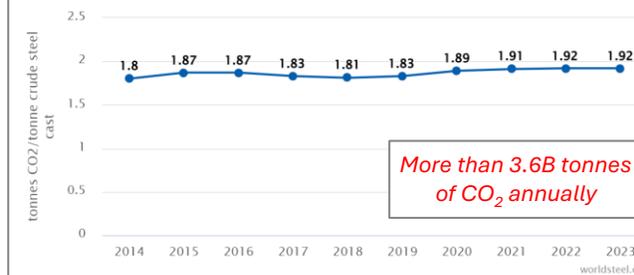
WorldSteel data<sup>2</sup> shows global crude steel production approaching 1.9 billion tonnes (1.84B in 2024<sup>3</sup>)

million tonnes, crude steel production



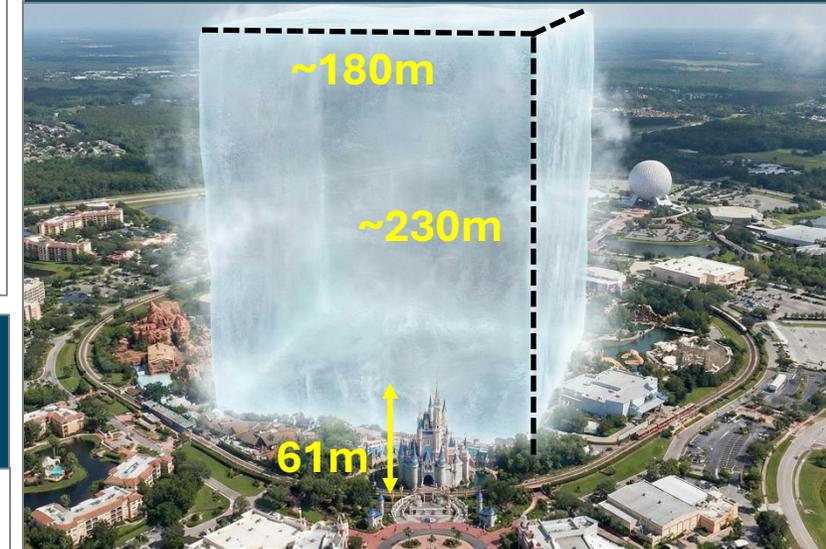
This is occurring at the same time the world average CO<sub>2</sub> intensity per tonne of steel shows marginal increase<sup>4</sup>

1. CO<sub>2</sub> emissions intensity



More than 3.6B tonnes of CO<sub>2</sub> annually

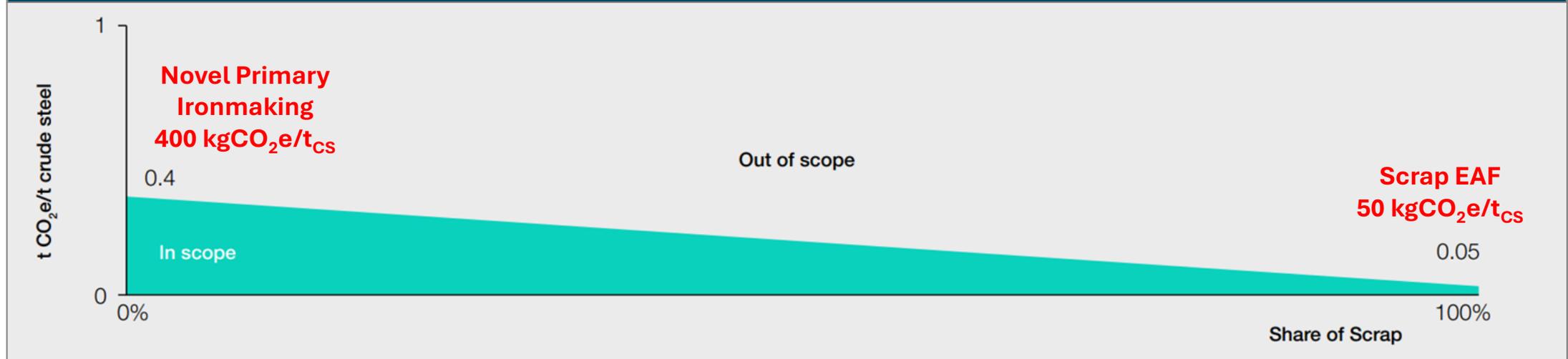
If annual iron and steel emissions were a block of dry ice - we'd make ~300 of these.





# Market Demand & Desire for Near Zero Steel

“Near zero” crude steels are defined on a sliding scale:  
less than 50 kgCO<sub>2</sub>e/t for 100% scrap based steel, and 400 kgCO<sub>2</sub>e/t for primary material (no scrap)<sup>1</sup>.



- 10% of annual steel procurement as NZS by 2030<sup>1</sup>
- Announced 2.3M in annual demand for NZS to date<sup>2</sup>



Formerly H<sub>2</sub> Green Steel

- Pre-sold 1.5 Mtpy<sup>3</sup> of near zero steel
- Plans for 5 Mtpy of steel production by 2030



- EU CBAM suggests 8-12 Mtpy of reduced imports to Europe from carbon border adjustments<sup>4</sup>



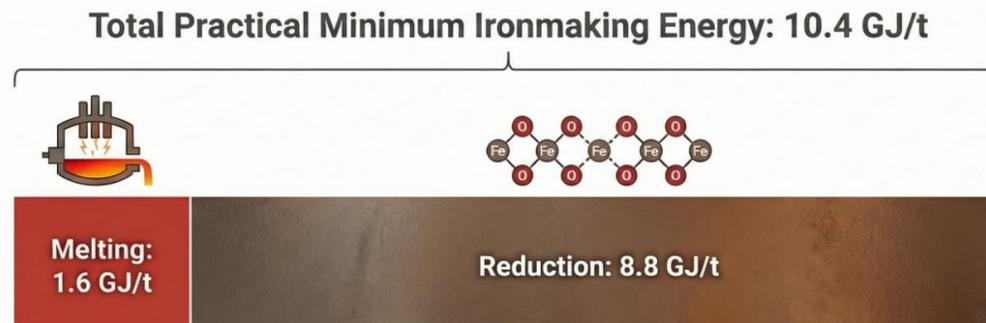
# Where Does Today's Metallic Iron Originate?

Compiled global estimate of different process energy intensities & CO<sub>2</sub> intensities from various sources<sup>1-5</sup>

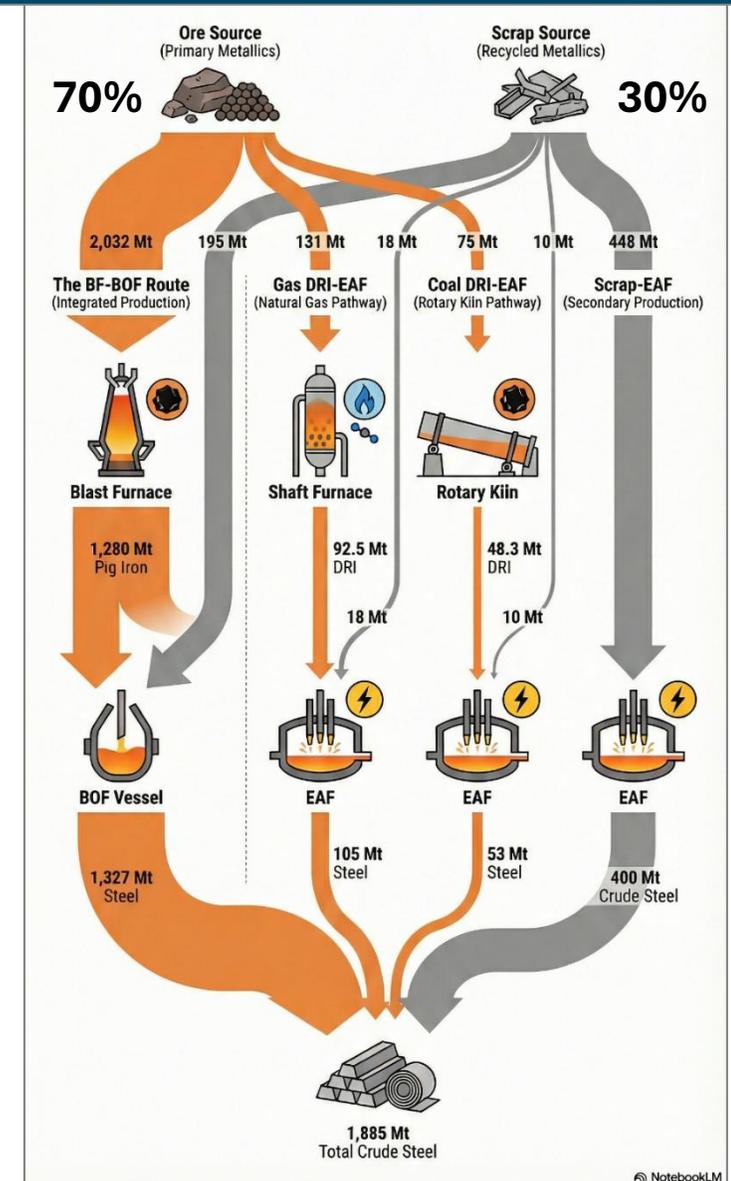
Production Route	Feedstock	Energy Intensity (GJ/tcs)	Total GHG Intensity (CO <sub>2</sub> e Scope 1, 2, 3)
<b>BF-BOF</b>	Iron Ore + Coal	21.4 - 22.7	2.66
<b>Gas-DRI-EAF</b>	Iron Ore + Nat. Gas	17.1 - 21.8	1.66
<b>Coal-DRI-EF</b>	Iron Ore + Coal	20.4 - 21.6	2.70 - 3.00
<b>Scrap-EAF</b>	100% Steel Scrap	2.1* - 5.2**	0.71
<b>Global Average</b>	Mixed	21.0	2.18

Different data definitions provide the range. At the low end, \*2.1 is an estimated site energy usage whereas \*\*5.2 is an equivalent "Primary Energy" assuming generation plant power losses.

Practical Minimum considers unavoidable energy required for impurities in the ore, scrap contaminants, and gas heat losses<sup>5</sup>. It does not consider sintering, cokemaking, or energy losses at the point of production for electricity. This is why there is a gap between global data, true thermodynamic minimums, and practical minimums.



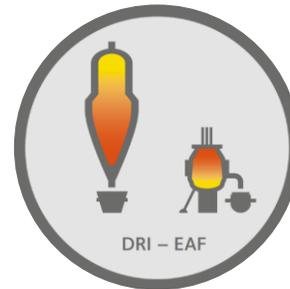
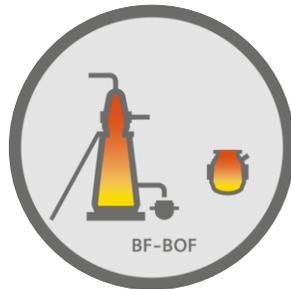
Illustrative AI generated global material flows pieced together from many sources<sup>1-5 & 6-13</sup>





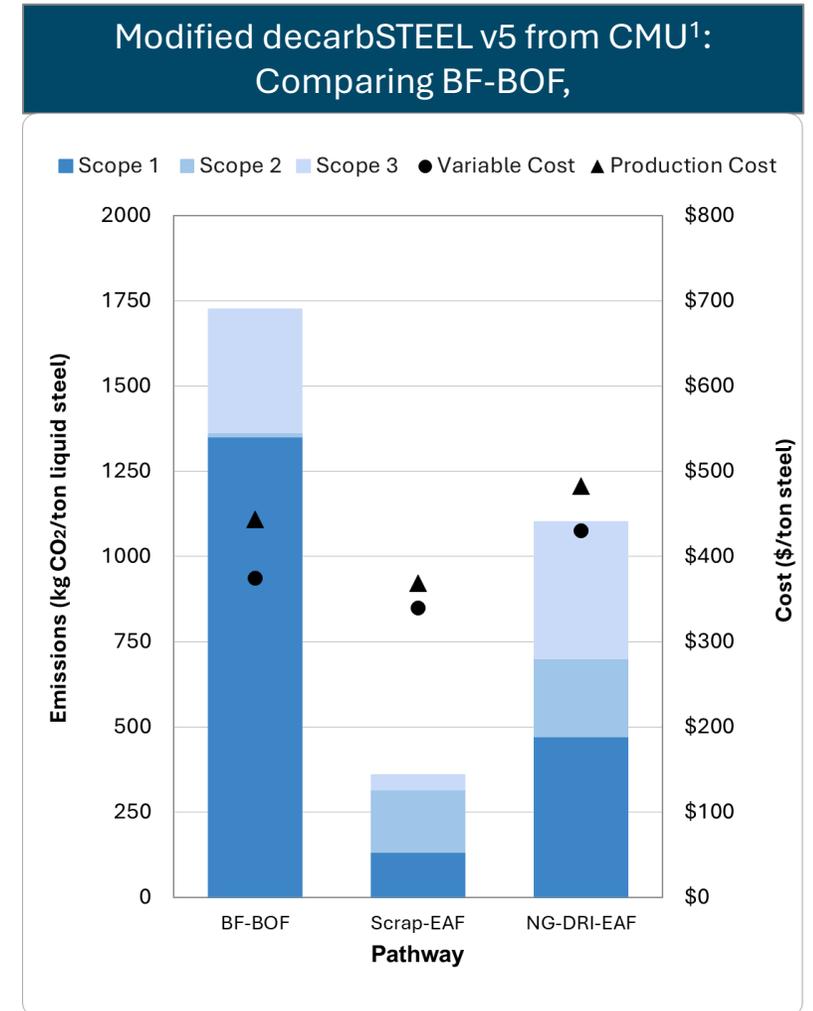
# Comparison of BAU Routes (North American Context)

- Shoutout to the **decarbSteel**<sup>2</sup> tool from CMU, funded in part by the AIST's **Sustainable Technologies for Steel Manufacturing Grant**<sup>3</sup>



Process Route:	BF-BOF	EAF	DRI-EAF
<b>Purpose &amp; Upside</b>	Counter-current reduction and smelting of high gangue ores	Efficient scrap melting & flexible operations	High grade ore reduction and melting for high quality steel
<b>Downsides</b>	Expensive integrated facility requiring high CAPEX and high CO <sub>2</sub>	Limited grade quality without high scrap control and metallic use	Limited feedstock flexibility because of EAF, needs low-cost NG
<b>Emissions Considerations</b>	<b>Scope 1:</b> Coal/coke <b>Scope 2:</b> Limited <b>Scope 3:</b> Lime, pellets, O <sub>2</sub>	<b>Scope 1:</b> Injection C <b>Scope 2:</b> Electricity <b>Scope 3:</b> Fluxes	<b>Scope 1:</b> NG <b>Scope 2:</b> Electricity <b>Scope 3:</b> Fluxes, pellets, NG

*\*\*Noted scope emissions are illustrative and not exhaustive, emphasizing the largest sources per category*

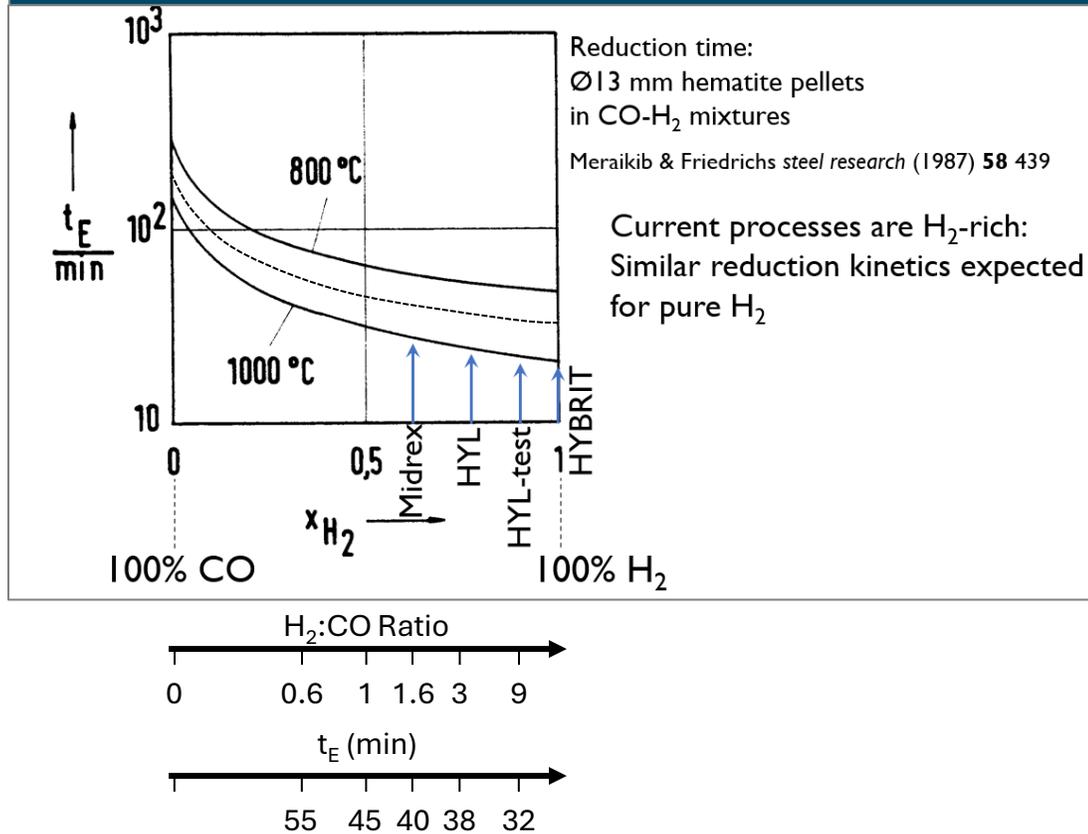




# Shaft Furnace - Key Levers & Opportunities

## Gas Composition Flexibility

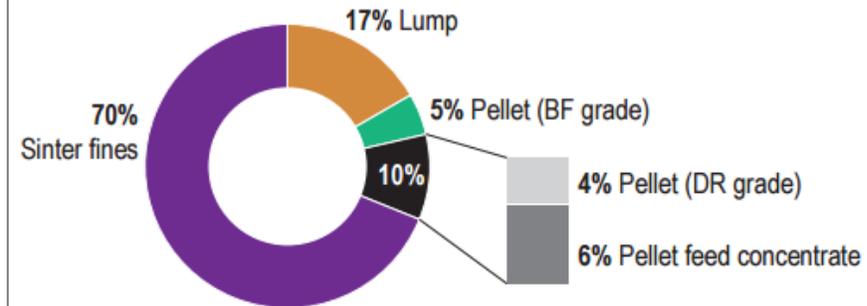
Data from Meraikib & Friedrichs<sup>1</sup> shows the difference in reduction rate by temperature and gas composition.



## Ore Grade Adaption (*Plant Dependent*)

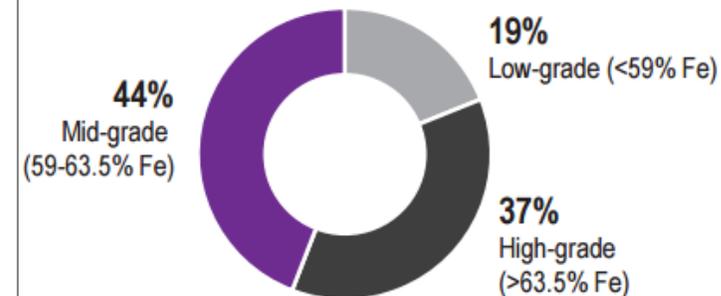
Fast Markets Research from 2021<sup>2</sup> highlights seaborne iron ore travels around the world.

### Global iron ore exports by product grade



While pellets are the primary focus of today's discussion, fluidized bed reduction is proven and usable for sinter fines to apply gas-based reduction to more feedstocks.

### Global iron ore exports by grade



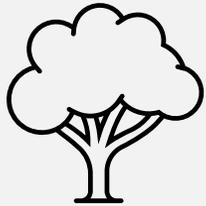
Including captive pellet plants, pellets make up about 24% of annual iron consumption globally<sup>2</sup>. Estimated at 597 Mtpy<sup>3</sup>.



# Hydrogen DRI – The Most Marketed Alternative

- Benefits from decades of shaft furnace experience
- Option for partial adoption in pre-existing DRI systems
- Nearest technologically viable alternative to pre-existing fossil fuel-based processes, barring CCS integration

## Why hydrogen?



No direct site emissions except water



Independence from fossil fuels



Fast reaction kinetics offer higher throughput

From Stegra<sup>1</sup>, installation of 200MW of electrolyzer capacity needed to supply H<sub>2</sub>. Targeting 740MW of capacity<sup>2</sup>.



90% of 3 Mile Island NPP<sup>3</sup>

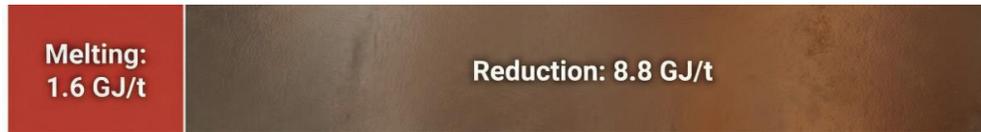


Roughly 8.5 EAFs producing 1.5 Mtpy steel

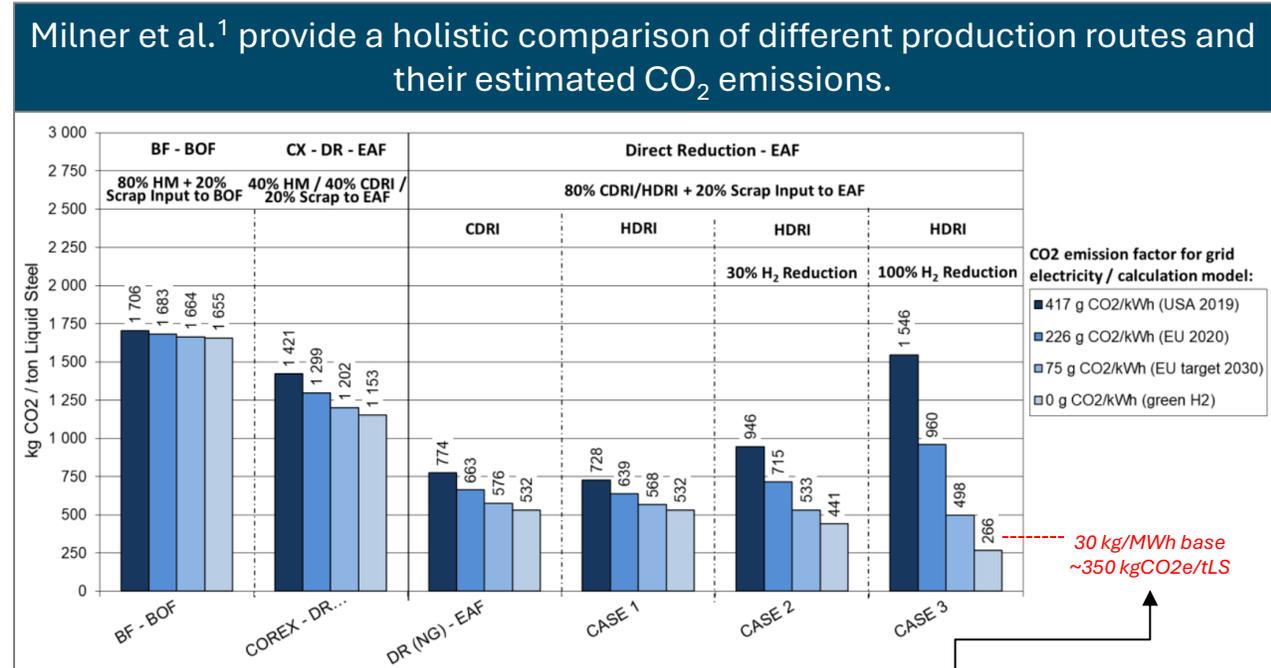


# Hydrogen DRI – Energy Usage & Emissions Sensitivity

**Must still supply energy to break Fe-O bonds, just a different sourcing mechanism**



- From an emissions perspective, H<sub>2</sub>-DRI competes with NG-DRI, using about 10.5 GJ/t<sub>DRI</sub><sup>1</sup>
  - NG combustion emissions: 50.15 kgCO<sub>2</sub>e/GJ<sub>NG</sub>
  - NG upstream emissions: 12.04 kgCO<sub>2</sub>e/GJ<sub>NG</sub> [fugitive methane]
  - Total emissions estimated per tDRI: 62.19 kgCO<sub>2</sub>e/GJ<sub>NG</sub>
  - Total DRI Emissions from NG: 653.00 kgCO<sub>2</sub>e/t<sub>DRI</sub>
- Reduction with H<sub>2</sub> requires about 58 kgH<sub>2</sub>/t<sub>DRI</sub>, implying 11.25 kg<sub>CO2e</sub>/kg<sub>H2</sub> as breakeven.
- What does this mean for grid-cleanliness to breakeven on electrolysis?
  - 55 kWh/kg<sub>H2</sub> = 3.19 MWh/t<sub>DRI</sub> PLUS ~1MWh gas heating
  - 653/4.19 = ~156 kg<sub>CO2e</sub>/MWh (**ceiling**)



**Reality:**

- “It Depends” as individual situations are highly regional
- We ultimately care about \$/tCO<sub>2</sub>e abated; emissions abatement cost is key

NREL<sup>2</sup> estimates total life cycle emissions of wind around 10 kg/MWh, solar PV 40 kg/MWh. Batteries alone are around 33 kg/MWh; combined residential PV+LI systems can be 85 kg/MWh<sup>3</sup>. Quebec, the gold standard of low CO<sub>2</sub> hydroelectric power, has full life cycle emissions of 34.5 kg/MWh<sup>4</sup>.



# Hydrogen DRI – Key Cost Drivers

Factoring in other process and embodied emissions, CO<sub>2</sub>e breakeven occurs around 100 kg/MWh

		Relative tCO <sub>2</sub> e per tSteel: H2-DRI-EAF minus NG-DRI-EAF									
		kgCO <sub>2</sub> e/kWh									
		0.00	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
kgH <sub>2</sub> /tDRI	46	-0.42	-0.34	-0.26	-0.18	-0.10	-0.02	0.18	0.38	0.59	0.79
	50	-0.42	-0.34	-0.25	-0.16	-0.08	0.01	0.23	0.45	0.66	0.88
	54	-0.42	-0.33	-0.24	-0.15	-0.05	0.04	0.27	0.51	0.74	0.97
	58	-0.42	-0.33	-0.23	-0.13	-0.03	0.07	0.32	0.57	0.82	1.07
	62	-0.42	-0.32	-0.21	-0.11	0.00	0.10	0.37	0.63	0.89	1.16

Strictly looking at economic performance, H2-DRI is only competitive at very low electricity costs

H2 Favored

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
kgH <sub>2</sub> /tDRI	46	-\$29	-\$6	\$17	\$40	\$62	\$85	\$108	\$131	\$154	\$176
	50	-\$28	-\$4	\$21	\$45	\$69	\$94	\$118	\$142	\$167	\$191
	54	-\$27	-\$1	\$25	\$50	\$76	\$102	\$128	\$154	\$180	\$206
	58	-\$26	\$1	\$28	\$56	\$83	\$111	\$138	\$165	\$192	\$219
	62	-\$26	\$3	\$32	\$61	\$90	\$119	\$148	\$177	\$206	\$235

NG Favored

At higher costs of natural gas, the opportunity for green H2 becomes larger.

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF (46 kgH <sub>2</sub> /tDRI)									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
NG \$/MMBtu	\$4	-\$14	\$9	\$31	\$54	\$77	\$100	\$123	\$146	\$169	\$192
	\$8	-\$38	-\$15	\$8	\$31	\$54	\$77	\$100	\$123	\$145	\$168
	\$12	-\$61	-\$38	-\$15	\$8	\$30	\$53	\$76	\$99	\$122	\$145
	\$16	-\$85	-\$62	-\$39	-\$16	\$7	\$30	\$53	\$76	\$99	\$121
	\$20	-\$109	-\$86	-\$62	-\$39	-\$16	\$6	\$29	\$52	\$75	\$98

H2 Favored

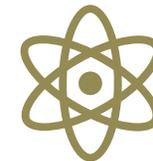
NG Favored

Considering change in steel emissions divided by change in steel cost estimates abatement cost.

		Abatement Cost (\$/tCO <sub>2</sub> e): H2-DRI vs. NG-DRI									
		kgCO <sub>2</sub> e/kWh									
		0.000	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
\$/kWh	\$0.02	\$40	\$50	\$65	\$95	\$172	\$958				
	\$0.04	\$148	\$183	\$240	\$348	\$634					
	\$0.06	\$256	\$316	\$415	\$602	\$1,095					
	\$0.08	\$364	\$450	\$589	\$855	\$1,556					
	\$0.10	\$471	\$583	\$764	\$1,108	\$2,018					

H2 Net Emitting

Nominal estimated cost of CO<sub>2</sub>e abatement for a H2 DRI to EAF using low emissions and low-cost power in a region like Quebec. NG-DRI-EAF offers \$62/t<sub>CO2e</sub> abatement versus BF-BOF w/ \$6.45/MMBtu NG.



H<sub>2</sub> DRI can work where electricity is readily available, at low cost and low emissions.

These regions are extremely limited globally and will end up going to first movers.

While nuclear power can achieve low-emissions power, it is too expensive to be cost competitive with natural gas.

Calculations assume 30-year plant life. Changing this changes CAPEX sensitivity for FOAK equipment.

There was an implicit assumption 5 years ago that power prices would continue falling. The rise of AI data centers suggests this will not occur.



# Biogenic Syngas DRI – Alternative Energy Sourcing

- The bioeconomy has seen it's share of stops and starts, and is undergoing another resurgence
- Ethanol has long been produced, and other forms of green chemicals are being developed like MeOH, backed by international companies like Maersk.

## Beaver Lake Renewables<sup>1</sup> is building a >500,000 metric ton per year green methanol from gasified biomass in Louisiana

The \$2.5 billion Beaver Lake Renewable Energy project utilizes SunGas S1000™ technology to repurpose forestry residues, converting waste into low-carbon marine fuel while permanently sequestering biogenic CO<sub>2</sub>.

### INPUT: SUSTAINABLE BIOMASS SOURCING

#### 2.5 Million Tons of Annual Feedstock

Sustainably sourced wood thinnings, tree-tops, and sawmill residues from local working forests.

#### The South's "Forestry Relief Valve"

Utilizes low-value wood residues that currently choke landowners and lack traditional markets.

### PROCESS: SUNGAS S1000™ GASIFICATION

Three standardized modular trains convert raw wood fiber into high-purity biogenic syngas.

### OUTPUT: CLEAN FUEL & CARBON REMOVAL

#### 500,000+ Tons of Green Methanol

Provides critical low-carbon fuel for global shipping fleets, including A.P. Moller – Maersk.

#### 1 Million Tons of CO<sub>2</sub> Sequestered

Biogenic carbon is captured and permanently stored in deep geologic formations in Louisiana.

#### PROJECT SCALE & IMPACT

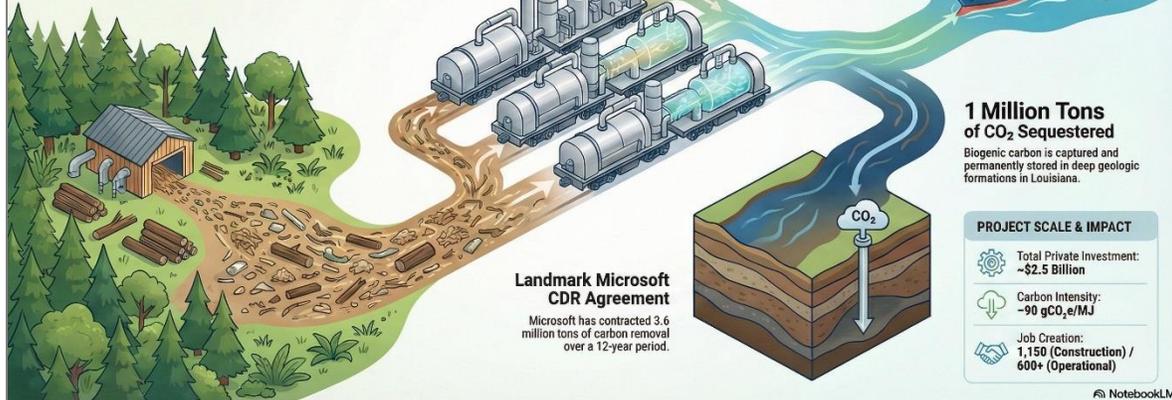
Total Private Investment: ~\$2.5 Billion

Carbon Intensity: ~90 gCO<sub>2</sub>e/MJ

Job Creation: 1,150 (Construction) / 600+ (Operational)

#### Landmark Microsoft CDR Agreement

Microsoft has contracted 3.6 million tons of carbon removal over a 12-year period.



NotebookLM

SunGas Renewables<sup>2</sup> is the technology provider for this gasification project. At 2.5M tpy of woody feedstock, you could run a 2Mtpy DRI facility.

### Take Complex Hydrocarbon Molecules



Forest Residue



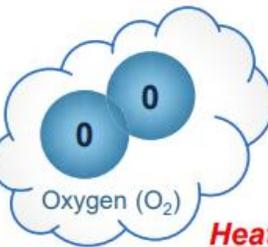
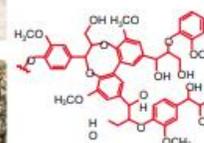
Agri Waste



MSW

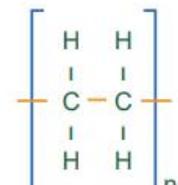


Plastic Waste

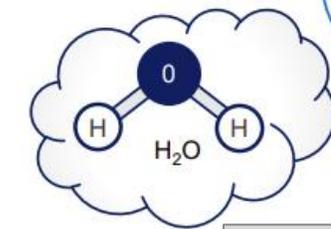


Oxygen (O<sub>2</sub>)

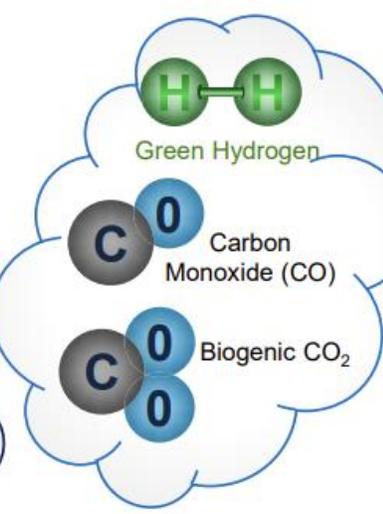
Heat



Polyethylene



H<sub>2</sub>O



Green Hydrogen

Carbon Monoxide (CO)

Biogenic CO<sub>2</sub>

Big biogenic projects are happening and pursuing co-product CDR.



# Charm Industrial: Bioenergy Industrialization & CO<sub>2</sub> Removal

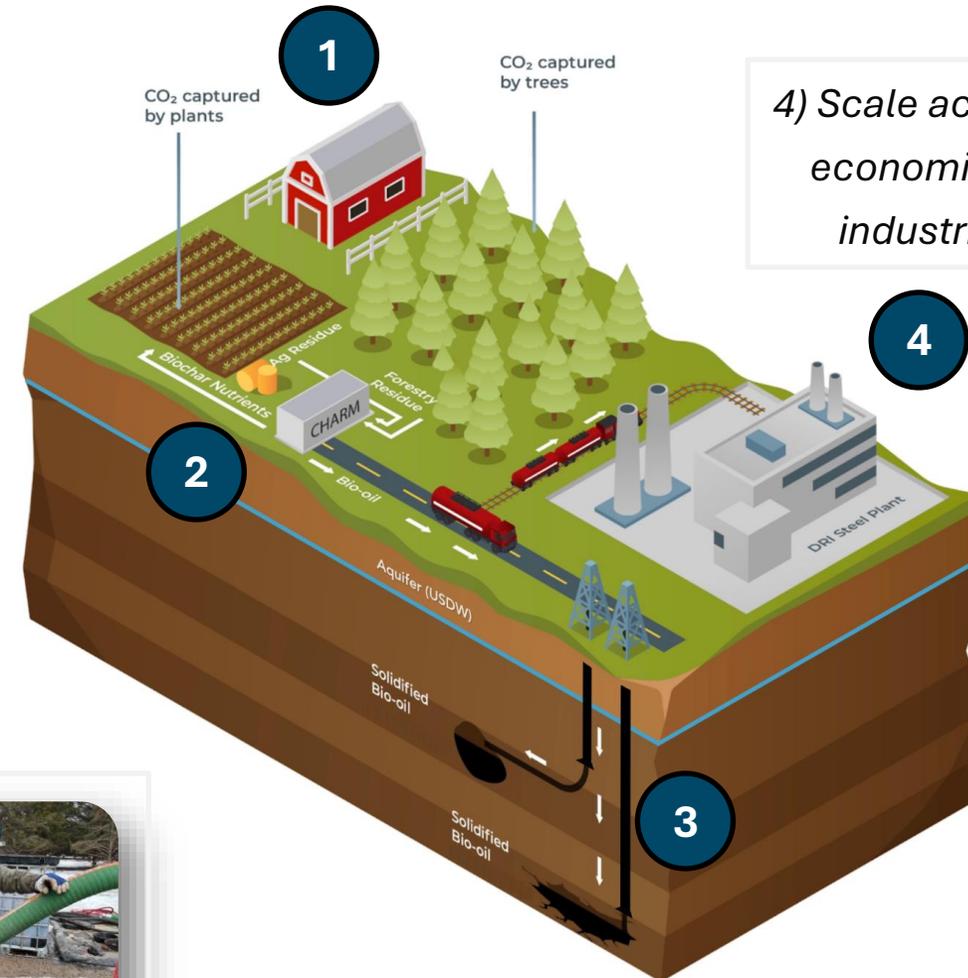
1) Charm uses plant residues from farms and forests



2) With heat and minimal oxygen, Charm converts biomass into biochar and bio-oil via pyrolysis



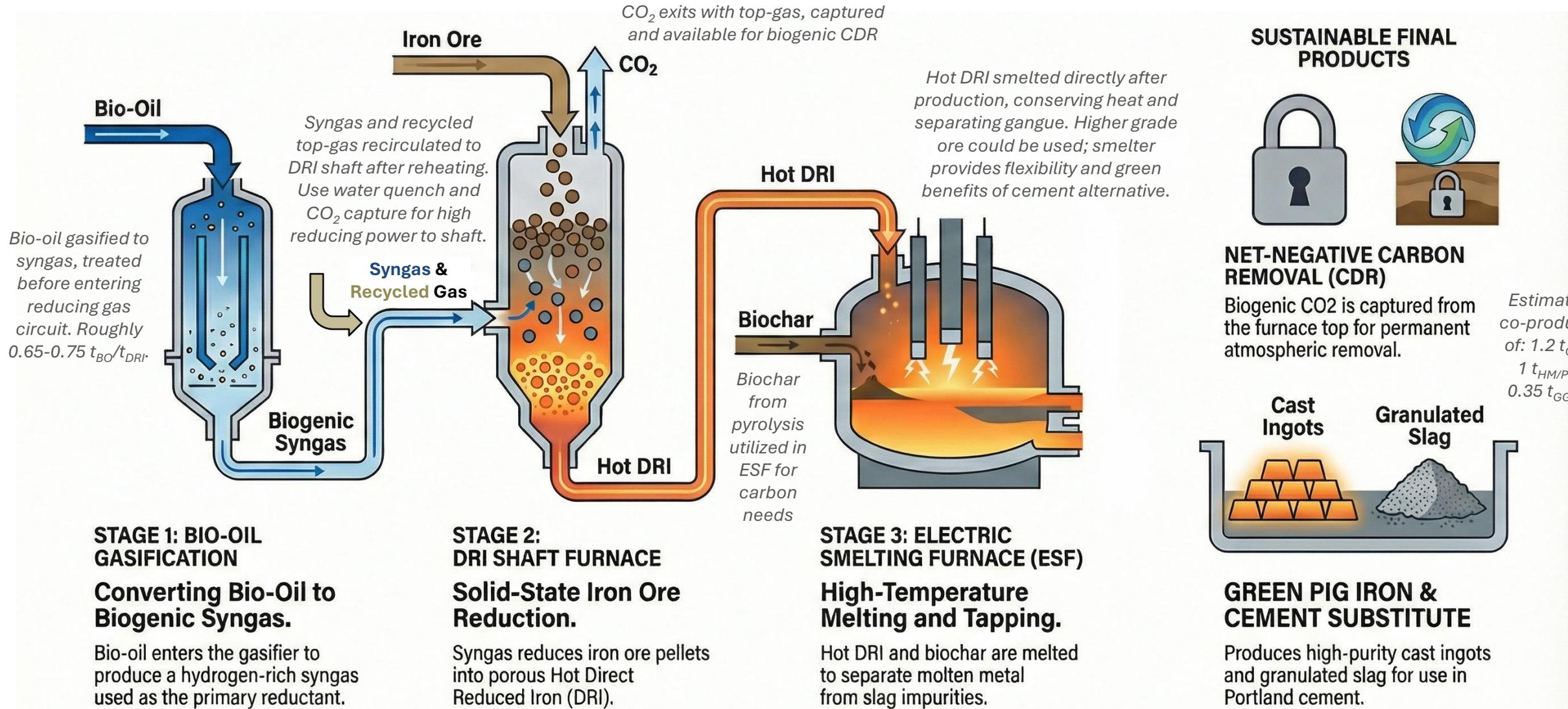
3) Charm injects the bio-oil deep underground for permanent carbon removal, and applies biochar on fields



4) Scale achieves suitable economics to support industrial activities



# Biogenic Syngas DRI – Schematic & Energy Flow



## STAGE 1: BIO-OIL GASIFICATION

### Converting Bio-Oil to Biogenic Syngas.

Bio-oil enters the gasifier to produce a hydrogen-rich syngas used as the primary reductant.

## STAGE 2: DRI SHAFT FURNACE

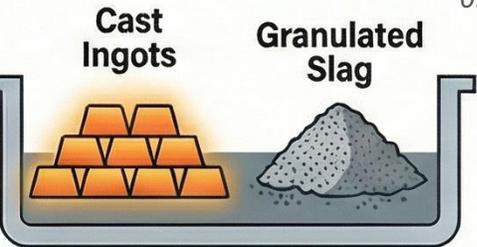
### Solid-State Iron Ore Reduction.

Syngas reduces iron ore pellets into porous Hot Direct Reduced Iron (DRI).

## STAGE 3: ELECTRIC SMELTING FURNACE (ESF)

### High-Temperature Melting and Tapping.

Hot DRI and biochar are melted to separate molten metal from slag impurities.



## GREEN PIG IRON & CEMENT SUBSTITUTE

Produces high-purity cast ingots and granulated slag for use in Portland cement.



# Biogenic Syngas DRI – Cost Drivers

## Biomass Sourcing



- Secure sufficient economical biomass to supply the gasification process.
- 1 Mtpy of DRI production requires<sup>1</sup>:
  - 1.1 Mtpy dry **wood**
  - 3.0 Mtpy dry **corn stover**

## Transportation



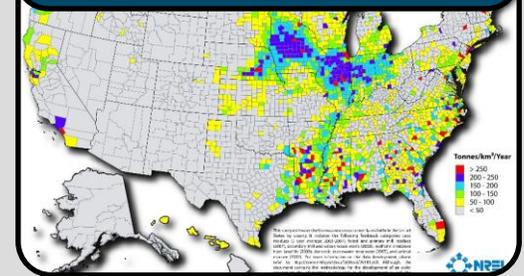
- Aggregate bio-oil at scale for gasification and DRI plant
- Achieve suitably low-cost rail economics
  - Bulk crude shipping rates are around \$0.06/t-mi<sup>2</sup>
    - Ex. \$30/t for 500mi

## Gasification TRL



- Replace reformer or electrolyzers with bio-oil gasifier. Instead of a NG-reformer the facility needs a gasifier and process gas heater, with CO<sub>2</sub> capture:
  - *MXCOL*
  - *Energiron w/ gasifier*
- Higher complexity means higher CAPEX (est. +50%) compared to Midrex base

## Regional Relevance



- Recognize that this approach is regionally limited to areas with biomass and CCS
- For CCS capabilities, require compression, transportation, and sequestration for supercritical CO<sub>2</sub>
  - Expect <\$50/t<sub>CO2</sub><sup>3</sup>

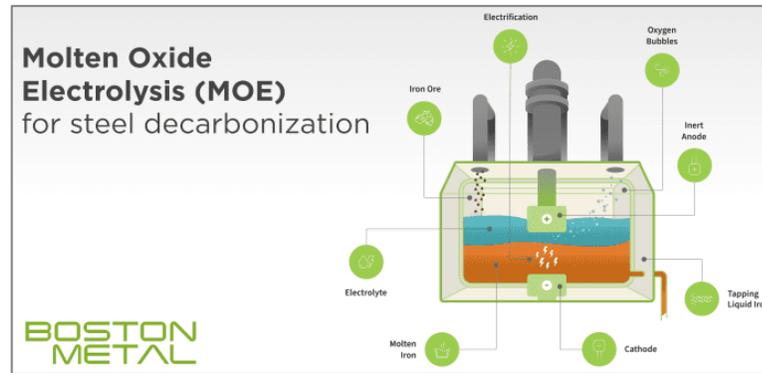


# Novel Ironmaking & Direct Electrification

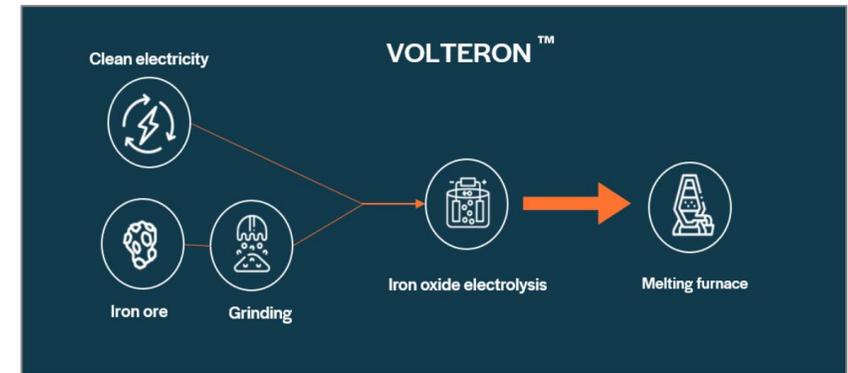
- Streamlined plant design and direct electrification may reduce total energy demands<sup>1</sup>
- Lower Technology Readiness Level (TRL) and under active development
  - **LT Electrowinning (Electra)**: 500 tpy demo by mid-2026, “commercial scale” by 2029<sup>2</sup>
  - **MOE (Boston Metal)**: Working on niobium first for higher value (2026), est. demo for steel by 2028<sup>3</sup>
  - **Volteron (ArcelorMittal & John Cockerill)**: 40-80ktpy by 2027<sup>4</sup>



**Reduction:** 9.4-10.8 GJ/t  
**Melting (EAF):** 1.4 GJ/t  
Total before losses: 10.8-12.2 GJ/t



**Reduction & Smelting:** 10.8 GJ/t  
Estimated Energy Losses: 20-30%  
Estimated total w/ losses: 13.5-15.4 GJ/t

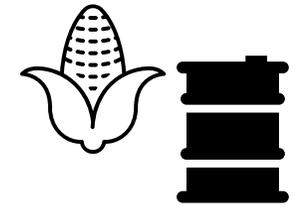
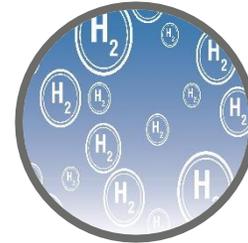
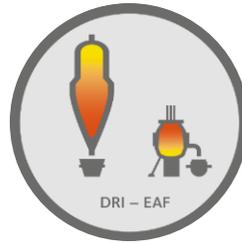


**Reduction:** 9.4 GJ/t (*demoed at pilot scale*)  
**Melting (EAF):** 1.4 GJ/t  
Total before losses: 10.8 GJ/t

Making a rough estimate, most of these processes likely end up near 15 GJ/t depending on final process design. This is an improvement over 15-20 GJ/t for H<sub>2</sub> DRI-EAF, but still a large energy load.



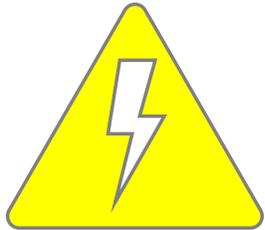
# Comparing the Pathways Forward



Process:	NG DRI	H2 DRI	Electrolysis+	Biogenic DRI
<b>Pros:</b>	<ul style="list-style-type: none"> <li>Available today</li> <li>Low-cost today</li> <li>Many improvement pathways (H<sub>2</sub> blend, CCS, reduced fugitive methane emissions)</li> </ul>	<ul style="list-style-type: none"> <li>Utilizes pre-existing DRI technology</li> </ul>	<ul style="list-style-type: none"> <li>Expected lowest energy requirement of all ironmaking technologies</li> </ul>	<ul style="list-style-type: none"> <li>Leverages pre-existing DRI facility concepts</li> <li>Co-produces 3 “green” products for future markets</li> </ul>
<b>Cons:</b>	<ul style="list-style-type: none"> <li>Emissions intensive compared with alternative low-CO<sub>2</sub> technologies</li> </ul>	<ul style="list-style-type: none"> <li>Requires electricity at a massive scale</li> <li>Requires electrolyzer mass deployment</li> <li>Requires carburization still for EAF operations</li> </ul>	<ul style="list-style-type: none"> <li>Requires electricity at a massive scale</li> <li>Requires carburization if EAF used</li> </ul>	<ul style="list-style-type: none"> <li>Requires sufficient low-cost biomass</li> <li>Technology risk associated with gasification</li> </ul>
<b>Expected Cost:</b>	<p><b>Low (2)</b> Assuming BF-BOF is the “low” benchmark</p>	<p><b>High (4)</b></p>	<p><b>Medium (3)</b> Lower energy requirement relative to H<sub>2</sub> DRI-EAF path</p>	<p><b>High (4)</b> CDR revenues can shift this price point lower.</p>



# Final Thoughts – No Shortage of Options & Choices



## Energy Reality

Ironmaking takes much more energy than steelmaking alone. Technological advances won't solve a thermodynamic limit.



## Transition Ready DRI

Adopting DRI-EAF today over BF-BOF can save ~400 kg<sub>CO<sub>2</sub>e</sub>/t before factoring in future improvement. That's 24Mt in 20 years.



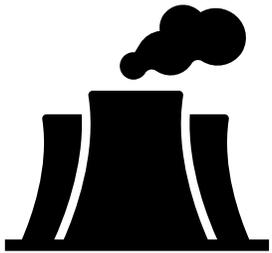
## Raw Materials

EAF alone will not be a solution, because primary iron is needed and most ore exceeds gangue limits for traditional EAFs.



## Regionality

Solutions are driven by regional energy pricing. Using natural gas today, and moving towards CCS, appears LCA favorable.



## Alternative Abatement & Carbon Dioxide Removal

Within 5 years we will see proof for <\$200/tCO<sub>2</sub> carbon removals at scale. However, it will not be able to satiate all of today's CO<sub>2</sub> emissions, so we need to balance the pathway between “good enough” economical decarbonization and CDR availability.



**Questions?**  
**Feel free to reach out!**

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# Bonus Slide: LNG Embodied Emissions (GWP100)

- The North American natural gas pricing situation is not globally common. Understanding the H2 DRI to NG DRI tradeoff in conditions where embodied emissions are higher and costs are higher is reviewed below.
  - Delivered LNG to NG costs are assumed to rise to ~\$9/GJ
  - Combustion emissions remain fixed at 50.15 kgCO<sub>2</sub>e/GJ, but Scope 3 emissions from methane slip and natural gas combustion during transportation rise to ~31.2 kgCO<sub>2</sub>e/GJ

Larger operating window for H2 from grid when greater embodied emissions of NG are considered.

		Relative tCO <sub>2</sub> e per tSteel: H2-DRI-EAF minus NG-DRI-EAF									
		kgCO <sub>2</sub> e/kWh									
		0.00	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
kgH <sub>2</sub> /tDRI	46	-0.56	-0.48	-0.40	-0.32	-0.24	-0.16	0.05	0.25	0.45	0.65
	50	-0.56	-0.47	-0.39	-0.30	-0.21	-0.12	0.09	0.31	0.53	0.75
	54	-0.56	-0.47	-0.37	-0.28	-0.19	-0.09	0.14	0.37	0.61	0.84
	58	-0.56	-0.46	-0.36	-0.26	-0.16	-0.06	0.19	0.43	0.68	0.93
	62	-0.56	-0.45	-0.35	-0.24	-0.14	-0.03	0.23	0.50	0.76	1.02

Green H2 becomes more favorable when NG price raised to \$9/GJ

H2 Favored

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
kgH <sub>2</sub> /tDRI	46	-\$47	-\$24	-\$1	\$22	\$45	\$67	\$90	\$113	\$136	\$158
	50	-\$46	-\$22	\$3	\$27	\$51	\$76	\$100	\$124	\$149	\$173
	54	-\$45	-\$19	\$7	\$33	\$58	\$84	\$110	\$136	\$162	\$188
	58	-\$44	-\$17	\$11	\$38	\$65	\$93	\$120	\$148	\$175	\$202
	62	-\$43	-\$15	\$14	\$43	\$72	\$101	\$130	\$159	\$188	\$217

NG Favored

Purely an economic consideration, this figure does not change since NG is sensitized.

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF (46 kgH <sub>2</sub> /tDRI)									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
NG \$/MMBtu	\$4	-\$14	\$9	\$31	\$54	\$77	\$100	\$123	\$146	\$169	\$192
	\$8	-\$38	-\$15	\$8	\$31	\$54	\$77	\$100	\$123	\$145	\$168
	\$12	-\$61	-\$38	-\$15	\$8	\$30	\$53	\$76	\$99	\$122	\$145
	\$16	H2 Favored	-\$62	-\$39	-\$16	\$7	\$30	\$53	\$76	NG Favored	\$121
	\$20	-\$108	-\$85	-\$62	-\$39	-\$16	\$6	\$29	\$52	\$75	\$98

When LNG is considered, abatement costs are about 50% lower combining higher emissions and cost.

		Abatement Cost (\$/tCO <sub>2</sub> e): H2-DRI-EAF minus NG-DRI-EAF									
		kgCO <sub>2</sub> e/kWh									
		0.000	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
\$/kWh	\$0.02	-\$1	-\$2	-\$2	-\$2	-\$3	-\$5				
	\$0.04	\$80	\$94	\$113	\$143	\$192	\$295				
	\$0.06	\$162	\$190	\$229	\$288	\$388	\$595				
	\$0.08	\$244	\$286	\$344	\$433	\$584	\$895				
	\$0.10	\$326	\$381	\$460	\$578	\$779	\$1,195				

H2 Net Emitting



# Bonus Slide: NG Embodied Emissions (GWP20)

- The standard LCA practice is to use GWP100, however, GWP20 is another standard recognizing that warming potential of methane on a 20-year basis is about 3x more impactful.
  - NG costs are assumed at \$6.45/MMBtu baseline (\$6.11/GJ)
  - Combustion emissions remain fixed at 50.15 kgCO<sub>2</sub>e/GJ, but Scope 3 emissions from methane slip and natural gas combustion during transportation rise to ~35 kgCO<sub>2</sub>e/GJ

Larger operating window for H2 from grid when greater embodied emissions of NG are considered.

		Relative tCO <sub>2</sub> e per tSteel: H2-DRI-EAF minus NG-DRI-EAF									
		kgCO <sub>2</sub> e/kWh									
		0.00	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
kgH <sub>2</sub> /tDRI	46	-0.59	-0.51	-0.43	-0.35	-0.26	-0.18	0.02	0.22	0.42	0.63
	50	-0.59	-0.50	-0.41	-0.33	-0.24	-0.15	0.06	0.28	0.50	0.72
	54	-0.59	-0.50	-0.40	-0.31	-0.22	-0.12	0.11	0.34	0.58	0.81
	58	-0.59	-0.49	-0.39	-0.29	-0.19	-0.09	0.16	0.41	0.65	0.90
	62	-0.59	-0.48	-0.38	-0.27	-0.17	-0.06	0.20	0.47	0.73	1.00

Direct economic comparison shows no change since the \$/GJ for NG has not changed.

H2 Favored

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
kgH <sub>2</sub> /tDRI	46	-\$29	-\$6	\$17	\$40	\$62	\$85	\$108	\$131	\$154	\$176
	50	-\$28	-\$4	\$21	\$45	\$69	\$94	\$118	\$142	\$167	\$191
	54	-\$27	-\$1	\$25	\$50	\$76	\$102	\$128	\$154	\$180	\$206
	58	-\$26	\$1	\$28	\$56	\$83	\$111	\$138	\$165	\$192	\$219
	62	-\$26	\$3	\$32	\$61	\$90	\$119	\$148	\$177	\$206	\$235

NG Favored

Purely an economic consideration, this figure does not change since NG is sensitized.

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF (46 kgH <sub>2</sub> /tDRI)									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
NG \$/MMBtu	\$4	-\$14	\$9	\$31	\$54	\$77	\$100	\$123	\$146	\$169	\$192
	\$8	-\$38	-\$15	\$8	\$31	\$54	\$77	\$100	\$123	\$145	\$168
	\$12	-\$61	-\$38	-\$15	\$8	\$30	\$53	\$76	\$99	\$122	\$145
	\$16	H2 Favored	-\$62	-\$39	-\$16	\$7	\$30	\$53	\$76	NG Favored	\$121
	\$20	-\$108	-\$85	-\$62	-\$39	-\$16	\$6	\$29	\$52	NG Favored	\$98

Higher embodied emissions for NG result in more favorable \$/tCO<sub>2</sub>e abated with H2.

		Abatement Cost (\$/tCO <sub>2</sub> e): H2-DRI-EAF minus NG-DRI-EAF									
		kgCO <sub>2</sub> e/kWh									
		0.000	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
\$/kWh	\$0.02	\$29	\$34	\$40	\$50	\$65	\$94				
	\$0.04	\$107	\$124	\$148	\$183	\$239	\$347				
	\$0.06	\$185	\$214	\$255	\$316	\$414	\$600				
	\$0.08	\$263	\$305	\$363	\$449	\$588	\$852				
	\$0.10	\$340	\$395	\$471	\$582	\$762	\$1,105				

H2 Net Emitting



# Bonus Slide: LNG Embodied Emissions (GWP20)

- Combining both assumption sets, NG costs are directly more expensive, and the associated CO2 impact is higher under the GWP20 scenario.
  - Delivered LNG to NG costs are assumed to rise to ~\$9/GJ
  - Combustion emissions remain fixed at 50.15 kgCO2e/GJ, but Scope 3 emissions from methane slip and natural gas combustion during transportation rise to ~75 kgCO2e/GJ

Large drift in grid emissions favorability considering high GWP20 from methane + LNG.

		Relative tCO2e per tSteel: H2-DRI-EAF minus NG-DRI-EAF									
		kgCO2e/kWh									
		0.00	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
kgH2/tDRI	46	-0.87	-0.79	-0.71	-0.63	-0.55	-0.47	-0.27	-0.06	0.14	0.34
	50	-0.87	-0.79	-0.70	-0.61	-0.52	-0.44	-0.22	0.00	0.22	0.43
	54	-0.87	-0.78	-0.69	-0.59	-0.50	-0.41	-0.17	0.06	0.29	0.53
	58	-0.87	-0.77	-0.67	-0.57	-0.47	-0.38	-0.13	0.12	0.37	0.62
	62	-0.87	-0.77	-0.66	-0.56	-0.45	-0.34	-0.08	0.18	0.45	0.71

Purely an economic consideration, this figure does not change since NG is sensitized.

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF (46 kgH2/tDRI)									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
NG \$/MMBtu	\$4	-\$14	\$9	\$31	\$54	\$77	\$100	\$123	\$146	\$169	\$192
	\$8	-\$38	-\$15	\$8	\$31	\$54	\$77	\$100	\$123	\$145	\$168
	\$12	-\$61	-\$38	-\$15	\$8	\$30	\$53	\$76	\$99	\$122	\$145
	\$16	H2 Favored	-\$39	-\$16	\$7	\$30	\$53	\$76	\$99	\$122	\$145
	\$20	-\$108	-\$85	-\$62	-\$39	-\$16	\$6	\$29	\$52	\$75	\$98

Green H2 becomes more favorable when NG price raised to \$9/GJ; no change to base LNG.

		Relative \$/tSteel Difference: H2-DRI-EAF minus NG-DRI-EAF									
		\$/kWh									
		\$0.00	\$0.01	\$0.02	\$0.03	\$0.04	\$0.05	\$0.06	\$0.07	\$0.08	\$0.09
kgH2/tDRI	46	-\$47	-\$24	-\$1	\$22	\$45	\$67	\$90	\$113	\$136	\$158
	50	-\$46	-\$22	\$3	\$27	\$51	\$76	\$100	\$124	\$149	\$173
	54	-\$45	-\$19	\$7	\$33	\$58	\$84	\$110	\$136	\$162	\$188
	58	-\$44	-\$17	\$11	\$38	\$65	\$93	\$120	\$148	\$175	\$202
	62	-\$43	-\$15	\$14	\$43	\$72	\$101	\$130	\$159	\$188	\$217

Considering LNG & GWP20 the relative abatement cost of CO2e drops significantly.

		Abatement Cost (\$/tCO2e): H2-DRI-EAF minus NG-DRI-EAF									
		kgCO2e/kWh									
		0.000	0.020	0.040	0.060	0.080	0.100	0.150	0.200	0.250	0.300
\$/kWh	\$0.02	-\$1	-\$1	-\$1	-\$1	-\$1	-\$2	-\$3	-\$13		
	\$0.04	\$52	\$57	\$64	\$72	\$82	\$97	\$172	\$776		
	\$0.06	\$104	\$115	\$128	\$145	\$166	\$195	\$347	\$1,564		
	\$0.08	\$157	\$173	\$193	\$218	\$250	\$294	\$522	\$2,353		
	\$0.10	\$209	\$231	\$257	\$291	\$334	\$392	\$697	\$3,141		

You're beginning to see nuclear power economics here, which combined with reduced energy demand from electrolytic process are probably quite favorable \$/tCO2e basis.

# Citations



# Citations (Page 1)

- **Coal & Natural Gas Exist – Why Talk About Alternatives?**

- [1] OurWorldInData, “Sector by sector: where do global greenhouse gas emissions come from?” (2020)
- [2] WorldSteel, “World Steel in Figures 2024”, (2024)
- [3] WorldSteel, “December 2024 crude steel production and 2024 global crude steel production totals”, (2025)
- [4] WorldSteel, “Sustainability Indicators 2024 Report”, (2024)

- **Market Demand & Desire for Near Zero Steel**

- [1] First Movers Coalition, “First Movers Coalition - Steel commitment” (2025)
- [2] World Economic Forum, “First Movers Coalition: 120 Commitments for Breakthrough Industrial Decarbonization Technologies” (2024)
- [3] H2 Green Steel Case Study OECD, “Stegra (formerly H2 Green Steel) Steel - Sweden” (2024)
- [4] Global Efficiency Intelligence, “The Impact of the EU CBAM on Global Steel Trade” (2025)

- **Where Does Today’s Metallic Iron Originate?**

- Sources for the table of energy use and CO<sub>2</sub> emissions
  - [1] Institute for Energy Economics and Financial Analysis, “Fact Sheet: The facts about steelmaking Steelmakers seeking Green Steel” (2022)
  - [2] World Steel Association, “Sustainability Indicators Report 2025,” (2025)
  - [3] Sponge Iron Manufacturers Association, “DRI Update,” (2024); <http://www.spongeironindia.com/images/publications/DRI%20UPDATE%20October-2024.pdf>
  - [4] The Energy & Resources Institute, “Financing the Decarbonization of the Steel Sector in India,” (2023)
  - [5] Fruehan et al., “Theoretical Minimum Energies To Produce Steel,” (2000)
- Additional sources for global mass flow figure
  - [6] World Steel Association, “World Steel in Figures 2025,” (2025)
  - [7] Midrex Technologies, “2024 World Direct Reduction Statistics,” (2025)
  - [8] Nduagu et al., “Comparative life cycle assessment of natural gas and coal-based directly reduced iron (DRI) production: A case study for India,” Journal of Cleaner Production 347 (2022)
  - [9] The Transition Accelerator, “Hydrogen and the Decarbonization of Steel Production in Canada,” (2023)
  - [10] US DOE, “Bandwidth Study on Energy Use and Potential Energy Savings Opportunities in US Iron and Steel Manufacturing,” (2015)
  - [11] Milner et al., “The Road to CO<sub>2</sub>-free Direct Reduction,” (2021)
  - [12] The Energy & Resources Institute, “Financing Decarbonization of the Secondary Steel Sector in India,” (2023)
  - [13] International Iron Metallurgy Association, “The Use of Hot Briquetted Iron (HBI) in the Blast Furnace (BF) for Hot Metal Production,” (2024)



# Citations (Page 2)

## • Comparison of BAU Routes (North American Context)

- [1] Hoffmann, Elina; Karplus, Valerie J.; Pistorius, P. Christiaan, “decarbSTEEL (Decarbonizing Steelmaking TechnoEconomic Evaluation) Tool” (2024) v5. Carnegie Mellon University. <https://doi.org/10.1184/R1/27119169.v5>
  - \*\*Adding ~24% emissions from upstream natural gas production (fugitive methane) adds about 91 kgCO<sub>2</sub>e/tSteel to the NG,DRI case (+39 kgCO<sub>2</sub>e/tSteel for BF, and +5.6 tCO<sub>2</sub>e/tSteel for scrap-EAF)
  - Modified CO<sub>2</sub>
- [2] Giordana Verrengia, “decarbSTEEL: From classroom to conference debut,” Carnegie Mellon University, Wilton E. Scott Institute for Energy Innovation (2025)
- [3] AIST, “Sustainable Technologies for Steel Manufacturing Grant,” (2024)
- **Note:** Diagrams of BF-BOF, EAF, DRI-EAF modified from: ArcelorMittal, “Climate Action Report 2,” (2021)

## • Shaft Furnace - Key Levers & Opportunities

- [1] M. Meraikib and H. A. Friedrichs, “Zur isothermen Reduktion von Eisenerzpellets mit Kohlenmonoxid, Wasserstoff und deren Gemischen”, Steel Research 58 (1987), pp. 439–445. Modifications adding processes added by C. Pistorius.
  - Thank you Chris Pistorius for flagging this figure!
- [2] Fast Markets, “Understanding the high-grade iron ore market”, (2021)
- [3] Midrex, “Direct from Midrex – Iron Ore for Direct Reduction: The Challenge Updated,” Direct from Midrex Q4 (2025)

## • Hydrogen DRI – The Most Marketed Alternative

- [1] Stegra, “A behind-the-scenes look at progress inside the green hydrogen plant in Boden”, LinkedIn post (2025); <https://www.linkedin.com/feed/update/urn:li:activity:7366109514154102787/>
- [2] Fuel Cell Works, “Stegra Gears Up: 740 MW Electrolyser Modules En Route to Boden”, (2025); <https://fuelcellworks.com/2025/05/06/clean-energy/stegra-gears-up-740-mw-electrolyser-modules-en-route-to-boden>
- [3] Wikipedia, “Three Mile Island Nuclear Generating Station”, (2026) – Using nameplate 820 MWe as the reference value
- **Note:** 1.5Mtpy steel, assuming 80% power on time at 400 kWh/tSteel, is equivalent to needing 750,000 MWh per year continuously. Per hour it’s about 85.6 MWh/hr, or 86 MW.  $740/86 = \sim 8.5$  EAFs



# Citations (Page 3)

- **Hydrogen DRI – Energy Usage & Emissions Sensitivity**

- [1] Milner et al., “The Road to CO<sub>2</sub>-free Direct Reduction,” (2021)
- [2] NREL, “Life Cycle Greenhouse Gas Emissions from Electricity Generation: Update,” (2021)
- [3] IEA Photovoltaic Power Systems Programme, “Environmental Life Cycle Assessment of Residential PV and Battery Storage Systems”, (2020)
- [4] HydroQuebec, “GHG emissions and Hydro-Québec electricity,” (2025); <https://www.hydroquebec.com/sustainable-development/specialized-documentation/ghg-emissions.html#:~:text=must%20consider%20emissions%20generated%20in,34.5%20g%20CO2%20eq%2FkWh>.
  - Swedish power is estimated to have lower CO<sub>2</sub> emissions from its grid because of a higher dependence on nuclear power and wind than Quebec, which is almost exclusively hydroelectric.
  - The lower usage of hydropower means lower methane emissions from submerged organic matter.
- [5] Fruehan et al., “Theoretical Minimum Energies To Produce Steel,” (2000)

- **Hydrogen DRI – Key Cost Drivers**

- *No net new sources. See **decarbSteel** tool for underlying data and assumptions. Changes were made to sensitize various costs and input drivers.*

- **Biogenic Syngas DRI – Alternative Energy Sourcing**

- [1] Rapides Parish Journal, “Beaver Lake Renewable Energy project poised to become major economic catalyst for Central Louisiana,” (2025)
- [2] SunGas Renewables, “Accelerating the Energy Transition,” European Gasification Summit (2025)

- **Charm Industrial: Bioenergy Industrialization & CO<sub>2</sub> Removal**

- No net new sources

- **Biogenic Syngas DRI – Schematic & Energy Flow**

- **Note:** *These estimates come from an array of internal Charm models and calculations. Their purpose is largely illustrative and should not be assumed fixed.*



# Citations (Page 4)

- **Biogenic Syngas DRI – Cost Drivers**

- [1] Estimates of bio-oil needs, and subsequently biomass needs, come from Charm’s mass balances. They can generally be reconstructed consider 10.5 GJ/tDRI as the baseline energy need, 70% CGE for bio-oil to syngas (but overall energy recovery of 80-85% considering heat recovery), then making conversions from bio-oil to dry biomass based on mass and energy balances. Stover volumes are higher because the whole oil is likely split into light and heavy ends, and only the heavy ends are usable for gasification. This essentially doubles overall biomass needs for the process after other conversion losses are considered.
- [2] Canadian National Railway, “2025 Annual Report – Selected Railroad Statistics – Unaudited,” (2025): <https://www.cn.ca/en/customer-centre/-/media/a1958ef6ca6f40ebb32aa2d354291ecb.ashx>
- [3] Global CCS Institute, “Cost of CO2 Storage,” (2025): <https://www.globalccsinstitute.com/wp-content/uploads/2025/12/Cost-of-CO2-Storage-1225.pdf>

- **Novel Ironmaking & Direct Electrification**

- [1] P.C. Pistorius, “Energy Requirements for Electrification of Ironmaking & Steelmaking,” Southern African Pyrometallurgy 2024, (2024)
- [2] Maria Galluci, “Electra announces deals with Meta, Nucor to scale its clean iron tech,” Canary Media (2025)
- [3] Sarah Shemkus, “Boston Metal forges path to commercialization for green steel process,” Canary Media (2025)
- [4] John Cockerill, “ArcelorMittal and John Cockerill announce plans to develop world’s first industrial scale low temperature, iron electrolysis plant,” (2023)

- **Comparing the Pathways Forward**

- No net new sources

- **Final Thoughts – No Shortage of Options & Choices**

- No net new sources